

APPROXIMATE SOLUTION OF THE LAMINAR BOUNDARY LAYER EQUATION FOR A NON-NEWTONIAN FLUID ON A PLATE

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The laminar boundary layer equations for a non-Newtonian fluid on a flat plate are reduced to Prandtl-Mises variables and solved approximately in quadratures. The velocity profiles and the resistance coefficients are given for certain values of  $n$ . Agreement with the results of exact calculations is good.

For a fluid satisfying the rheological power law

$$\tau = K \left( \frac{\partial u}{\partial y} \right)^n, \quad (1)$$

the laminar boundary layer equations on a flat plate, in dimensionless form, are [1]

$$u_1 \frac{\partial u_1}{\partial x_1} + v_1 \frac{\partial u_1}{\partial y_1} = \frac{\partial}{\partial y_1} \left( \frac{\partial u_1}{\partial y_1} \right)^n, \quad \frac{\partial u_1}{\partial x_1} + \frac{\partial v_1}{\partial y_1} = 0, \quad (2)$$

where

$$\begin{aligned} x_1 &= \frac{x}{L}, & y_1 &= \frac{y}{L} R^{\frac{1}{1+n}}, \\ u_1 &= \frac{u}{U}, & v_1 &= \frac{v}{U} R^{\frac{1}{1+n}}, \\ R &= \frac{\rho U^{2-n} L^n}{K}. \end{aligned} \quad (3)$$

The boundary conditions are

$$\begin{aligned} \text{when } y_1 = 0 & \quad u_1 = 0, \quad v_1 = 0; \\ \text{when } y_1 = \infty & \quad u_1 = 1. \end{aligned} \quad (4)$$

Introducing the stream function  $\psi_1$ , we replace the second equation of (2) by the relations

$$u_1 = \frac{\partial \psi_1}{\partial y_1}, \quad v_1 = -\frac{\partial \psi_1}{\partial x_1}. \quad (5)$$

We shall pass from  $x_1, y_1$  to the new independent variables  $x_1, \psi_1(x_1, y_1)$ —Prandtl-Mises variables [2], and transform the first equation of (2) into these variables. Thus, it now takes the form

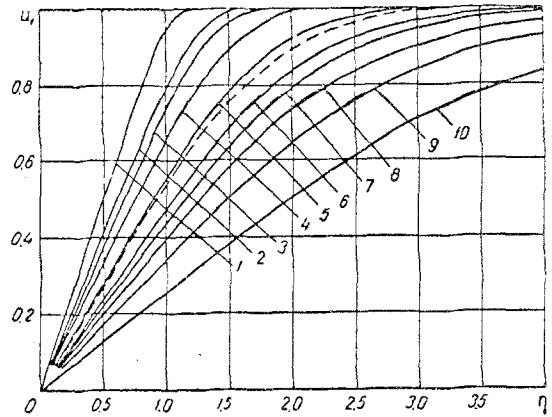
$$\frac{\partial z}{\partial x_1} = \sqrt{2z} \frac{\partial}{\partial \psi_1} \left( \frac{\partial z}{\partial \psi_1} \right)^n, \quad (6)$$

where we have designated

$$z = u_1^2/2. \quad (7)$$

Taking the straight line  $y_1 = 0$  as the zero stream line ( $\psi_1 = 0$ ), we write the boundary conditions (4), taking (7) into account, as

$$\begin{aligned} \text{when } \psi_1 = 0 & \quad z = 0; \\ \text{when } \psi_1 = \infty & \quad z = 1/2. \end{aligned} \quad (8)$$



Velocity distributions in the boundary layer with: 1)  $n = 3$ ; 2) 2; 3) 1.67; 4) 1.33; 5) 1.0; 6) 0.7; 7) 0.7; 8) 0.6; 9) 0.5; and 10) 0.3.

If  $z$  is regarded as being a function of only one variable

$$\zeta = \psi_1 [\sqrt{2} n (1+n) x_1]^{-1/(1+n)}, \quad (9)$$

then (6) becomes the ordinary differential equation

$$-\zeta = \sqrt{z} (z')^{n-2} z'' = \frac{\sqrt{z}}{n-1} \frac{d}{d\zeta} (z')^{n-1}, \quad (10)$$

where the primes denote differentiation with respect to  $\zeta$ .

The boundary conditions (8) are

$$\begin{aligned} \text{when } \zeta = 0 & \quad z = 0; \\ \text{when } \zeta = \infty & \quad z = 1/2. \end{aligned} \quad (11)$$

Equation (10) is easily integrated, if we put  $z = z_0 = 1/4$  as a zeroth-order approximation (under the square root), i. e., half of its value at the outer edge of the boundary layer, as was done in [3]. We then obtain the equation

$$-\zeta = \frac{1}{2} (z')^{n-2} z'' = \frac{1}{2(n-1)} \frac{d}{d\zeta} (z')^{n-1}, \quad (12)$$

which was examined in [4, 5] for  $n < 1$  in connection with the problem of unsteady motion of a non-Newtonian fluid on an infinite plate.

For  $n = 1$  (Newtonian fluid), the solution of (12) with boundary conditions (11) has the form

$$z = \frac{1}{2} \frac{2}{\sqrt{\pi}} \int_0^\zeta \exp(-\zeta^2) d\zeta = \frac{1}{2} \operatorname{erf} \zeta. \quad (13)$$

Comparison of the Approximate and Exact Solutions

$n$	$C$	$z'(0)$	$B_n$	$B_n$ [1]	$B_n$ [6]	Error, %
3/1 = 3	0.4502	0.9488	0.2043	0.1941	—	5.2
2/1 = 2	0.8256	0.8256	0.3277	0.3224	—	1.6
5/3 ≈ 1.67	1.250	0.7602	0.4015	—	—	—
3/2 = 1.5	1.697	0.7200	0.4490	0.4378	—	2.6
7/5 = 1.4	2.160	0.6956	0.4828	—	—	—
4/3 ≈ 1.33	2.631	0.6742	0.5070	—	—	—
6/5 = 1.2	4.565	0.6341	0.5643	—	—	—
1	—	—	0.6709	0.6641	0.6642	1.0
4/5 = 0.8	5.782	0.4835	0.8152	—	0.8109	0.5
7/9 ≈ 0.78	5.311	0.4743	0.8350	—	—	—
3/4 = 0.75	4.851	0.4623	0.8601	—	—	—
5/7 ≈ 0.71	4.407	0.4446	0.8944	—	—	—
3/5 = 0.6	3.631	0.3935	1.019	—	1.017	0.2
1/2 = 0.5	3.404	0.3451	1.152	1.151	1.151	0.1
1/3 ≈ 0.33	3.674	0.2608	1.435	—	—	—

For  $n \neq 1$ , integrating (12) twice, and taking the first condition of (11) into account, we find

$$z = \int_0^{\zeta} [(n-1)(C-\zeta^2)]^{\frac{1}{n-1}} d\zeta. \quad (14)$$

The arbitrary constant  $C$  for  $n < 1$  is determined from the second condition of (11), and for  $n > 1$  from the condition

$$\text{when } \zeta = \zeta_0, z' = 0, z = 1/2, \quad (15)$$

where  $\zeta_0$  is the value appropriate to the finite thickness of the boundary layer [1, 5].

The integral (14), as an integral of a binomial differential, may be expressed in finite form only for certain values of  $n$ .

In view of (7), the velocity profiles are calculated from the formula

$$u_1(\zeta) = \sqrt{2z(\zeta)}. \quad (16)$$

From (5) and (9) it follows that

$$\eta = y_1 [\sqrt{2n(1+n)} x_1]^{-\frac{1}{1+n}} = \int_0^{\zeta} \frac{d\zeta}{u_1(\zeta)}. \quad (17)$$

Equations (16) and (17) give the parametric relation between  $u_1$  and  $\eta$ .

The calculated velocity profiles are shown in the figure. Also shown, is the curve corresponding to the exact solution of the Blasius equation [2] (dashed curve,  $n=1$ ); its difference from the approximation is less than 4%.

With the aid of (1), (3), (5), and (9) let us determine the local frictional drag of the plate

$$c_f = 2\tau_w/\rho U^2 = B_n/R_x^{1/(1+n)}, \quad (18)$$

where

$$B_n = 2 [\sqrt{2n(1+n)}]^{-n/(1+n)} [z'(0)]^n, R_x = \rho U^{2-n} x^n/K. \quad (19)$$

The quantities required in calculating the velocity profiles and drag are given in the table.

The table also shows a comparison of some of the values  $B_n$  obtained in the present paper with the exact data of the authors of [1] and [6]. From the good agreement of these quantities and of the velocity profiles for  $n = 1$  the conclusion may be drawn that the first approximation used in solving Eq. (10) is adequate for practical purposes.

#### NOTATION

$\tau$ —frictional stress,  $\tau_w$ —the same at the wall;  $K, n$ —rheological characteristics of fluid;  $x$ —longitudinal coordinate;  $y$ —transverse coordinate;  $u, v$ —projection of velocity vector on  $x$  and  $y$  axes, respectively;  $U$ —velocity of external stream;  $L$ —characteristic length;  $R$ —Reynolds number;  $R_x$ —local Reynolds number.

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